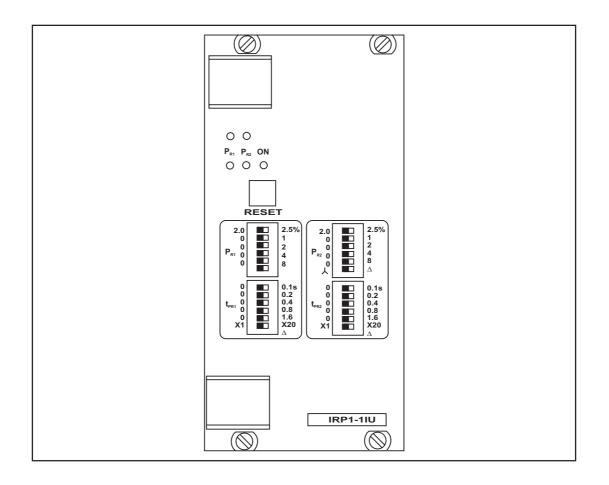


IRP1 - Directional Power Relay







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1. Introduction and application

When compared with traditional protection systems the protective relaying with IR - relays offer several advantages.

IR - protection relays are based on microprocessor and some on analog technique. They present our low priced protection relay generation and are used for all basic protection applications.

The following properties of the IR-protection relays, such as :

- Integration of multiple protection functions into one compact housing.
- User friendly setting procedure by means of DIP switches.
- Compact design due to SMD technique.

These are their superiority over the traditional protection systems.

All relays of this HIGH TECH RANGE are available for through panel mounting and in 19" racks. Connection terminals are of plug in type. All IEC/DIN regulations required for the individual application are reliably met by this relay.

The directional power relay **IRP1** is used for reverse power or forward power supervision in low voltage and medium voltage systems. The relay may be used for active power or reactive power application. The load is measured in one phase only on assumption that the phases are loaded symmetrically.

Among other applications the relay can be used as directional power relay for protection against reverse

power forward power of Turbo generators and Diesel generating sets if prime mover fails.

For the generator operating in parallel with a mains or another generator, it is imperative to supervise the power direction. If for example the prime mover fails the alternator operate as a motor and drive the prime mover (Diesel engine/Turbine). The **IRP1** recognises the power direction and switches off the alternator. This way, power losses and damages to the prime mover are avoided.

2. Features and characteristics

- Static protection relay
- Directional power measuring unit P_{R1} and P_{R2}.
- Sensitive power measuring with fine graded adjustment
- Separate adjustable trip delay for P_{R1} and P_{R2}.
- Phase shifting adjustment.
- Wide operating ranges of the supply voltage (AC/ DC).
- Plug in technology with self-shorting CT circuits.
- Coding plug for presetting of LED indications and the trip relays.
- Codable additional phase shifting.

3. Design

3.1 Connections

The connection diagrams are given in the fig. 3.1 and fig. 3.2.

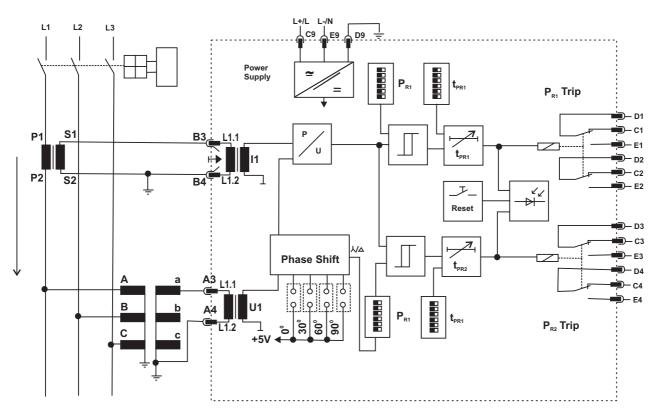


Fig. 3.1: Connection diagram IRP1 for phase to neutral supply voltage

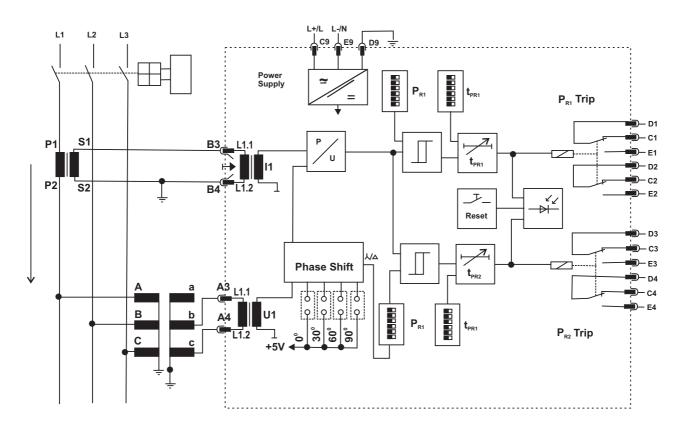


Fig. 3.2: Connection diagram for phase to phase supply voltage

3.2 Analog input circuits

The analogue input signal of the phase current I_{L1} , is led to the protection relay via B3- B4. The phase-tophase or phase-to-neutral voltage are connected via terminals A3 - A4. For medium voltage and high voltage systems a voltage transformer is needed for this. The system voltage of low voltage systems can be connected directly to the measuring inputs.

3.3 Output relays

The **IRP1** is equipped with two trip relays each with two change-over contacts:

- P_{R1} Tripping relay : C1, D1, E1 and C2, D2, E2
- P_{R2} Tripping relay : C3, D3, E3 and C4, D4, E4

3.4 Front plate

The front plate of the protection relay **IRP1** comprises the following operation indication elements:

- 4 DIP switches for the setting of the tripping values and times
- 5 LEDs for pick up/trip indication and readiness for service
- 1 pushbutton <RESET>

The detail of the front plate the relay IRP1 is shown in the fig. 3.3.

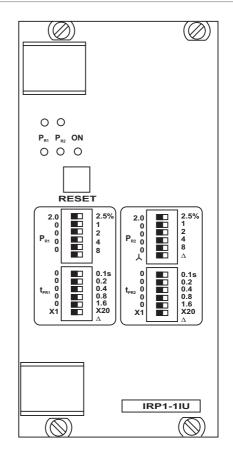


Fig. 3.3: Front plate

3.5 LEDs

There are 5 LEDs at the front plate of the protective relay IRP1 which indicate the following operational modes:

- Readiness for operation, LED ON (green)
- Pickup of PR1, upper LED ON (yellow)
- Pickup of PR2, upper LED ON (yellow)
- Trip of PR1, lower LED ON (red)
- Trip of PR2, lower LED ON (red)

3.6 <RESET> Push button

Pushbutton <RESET> is used for acknowledgement and reset after fault clearance.

The LEDs and output relays which are encoded for latching must be reset manually by pressing the pushbutton <RESET>.

4. Relay adjustment

4.1 Code jumpers

There are 4 code jumpers behind the front plate of the **IRP1** at the lower part for presetting the LED indications and the trip behaviour of the output relays.

The yellow pickup LEDs cannot be coded, they light up as soon as the setting value is exceeded and extinguish automatically when the setting value is fall short. Before leaving the factory, all code jumpers are pluged into their sockets.

The coding sockets are allocated to the functions as follows:

- Coding socket 1 + 2 = Reverse power tripping P_{R1}.
- Coding socket 3 + 4 = Reverse power tripping P_{R2}.

The position of the coding socket is shown in the fig. 4.3 and the function of the relay with different coding jumper adjustment is given in the Table 4.1 below

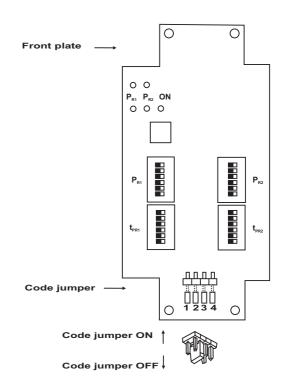


Fig. 4.3: Code jumper/socket

Code jumper	Junction	Code jumper position	Mode
1	Reverse power indication P _{R1}	OFF	latching of red LED P_{R1}
		ON	automatic reset of red LED $P_{_{R1}}$
2	Reverse power tripping P _{R1}	OFF	latching of trip relay P _{R1}
		ON	automatic reset of trip relay P _{R1}
3	Reverse power indication P _{R2}	OFF	latching of red LED P_{R2}
		ON	automatic reset of red LED P _{R2}
4	Reverse power tripping P _{R2}	OFF	latching of trip relay P _{R2}
		ON	automatic reset of trip relay P_{R2}

Table 4.1: Function of code jumpers

4.2 Y/Δ switch adjustment

IRP1 relay can be used for active or reactive directional power protection.

For desired application (Active/Reactive), the phase shift is required to be adjusted with the help of X11 jumper and Y/ Δ Dip switch adjustment. The connection shall be made as per the fig. 3.1 or fig. 3.2.

When connecting voltage inputs phase to neutral voltage, the current vector I_{L1} is parallel to the voltage vector U_{IN} .

For forward active power application, Y/Δ Dip switch must be at Y position and X11 jumper position at 0°.

For reverse active power application, Y/ Δ Dip switch must be at Δ position and X11 jumper position at 90°.

For reverse reactive power application, Y/Δ Dip switch must be at Y position and X11 jumper position at 90°.

When connecting voltage inputs to phase to phase voltage, the current vector I_{L1} is perpendicular to voltage vector U_{23} .

For forward active power application, Y/Δ Dip switch must be at Y position and X11 jumper position at 90°.

For forward reactive power application, Y/ Δ Dip switch must be at Y position and X11 jumper position at 0°.

For reserve reactive power application, Y/ Δ Dip switch must be at Δ position and X11 jumper position at 90°.

Using the voltage and current for other phases, the above mentioned application can be achieved by making proper phase shift adjustment.

4.3 Coding of phase shifter

Phase shifting between current and voltage can be adjusted from 0 to 90° by 30° steps. Consequently the actual phase shifting (dependent on the connection Y/

 Δ DIP switch and related phase shifting) is increased by the set value. In this manner a certain characteristical angle can be preadjusted. So, the maximum sensitivity of the relay can be set to $\cos \varphi = 0.87$ and 0.5 inductive or capacitive. Together with Y/ Δ DIP switch adjustment any phase shifting between 0° - 180° is possible in 30° steps between current and voltage. This can be helpful if, for instance, U_{1N} or U₂₃ are not available for measuring. It is also possible to use currents and voltages of other phases. In such a case sketching of a vector diagram is very useful.

The four coding facilities X11 jumper are on the PCB left to the front plate, shown in the fig. 4.4.

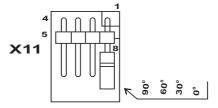


Fig. 4.4: Code jumpers for phase shifting

There is no phase shift adjusted with the initial adjustment (0°), i.e. coding plug applied one, two or three positions further to the left this means the phase is shifted 30°, 60° or 90°. The trip function is blocked if either a second coding plug is applied or there is no coding plug at all. The total phase shifting together with Y/Δ DIP switch and X11 jumper are mentioned in the Table 4.2.

Y/Δ	Adjustment	Angular displacement
		between I_{L1} and U_{1N}
	0°	0°
Y	30°	30°
	60°	60°
	90°	90°
	0°	90°
Δ	30°	120°
	60°	150°
	90°	180°

Table 4.2 : Phase shifting with DIP Switch and Jumper.

5 Working principle

The IRP1 is provided with two output relays $\rm P_{R1}$ and $\rm P_{R2}$, having separate adjustable pickup values and trip delays.

Measuring principle:

Voltage and current measured are galvanically decoupled via the input CT. Dependent on relay connection (Y or Δ) and encoding, either phase-to-neutral voltage U_{1N} or phase-to-phase voltage U₂₃ is used as reference voltage for load calculation. Current is measured in phase L1.

For the *IRP1* a stable system voltage is required. The load is calculated by evaluating value and phase angle of the current. If the set thresholds P_{R1} or P_{R2} are exceeded, the respective supervision circuit picks up and the corresponding LED lights up yellow. After the set trip delay has elapsed, the relay trips and respective LED lights up red.

5.1 Calculation of the setting value

Should the relay, for instance, trip at a generator reverse power of 10 %, this does not mean that the setting value of the *IRP1* is 10 %. Based on the transformer transformation ratio, the switching point has to be calculated.

The *IRP1* measures the power in one phase of the transformer secondary side. The power is assumed to be symmetrical.

The generator phase power must be related to the transformers secondary side.

Essential data

$S_{_{\rm G}}$ [kVA]	rated generator apparent power
cos(φ):	rated generator power factor
ln:	rated current of IRP1
Un:	rated voltage of IRP1
n, :	transformation ratio of the CT

 n_{ii} : transformation ratio of the VT

Connection of the *IRP1* to phase-to-phase voltage:

Conversion of the generator phase power $\rm P_{GS}$ based on the CT secondary side:

$$P_{GS} = \frac{S_{G} \cos(\phi)}{\sqrt{3}.n_{u}.n_{i}}$$

With the permissible generator reverse power $P_{_{RG}}$, the setting value $P_{_{R}}$ is then calculated as follows:

$$P_{R>}(\%) = \frac{\frac{S_{G} \cos(\phi)}{\sqrt{3.n_{u}.n_{i}}}}{U_{n}.l_{n}} \cdot P_{RG}(\%)$$

Calculation example 1: Medium voltage 10 kV

- generator apparent power: S_G = 1875 kVA
- rated power factor: $\cos(\phi) = 0.8$
- rated voltage of IRP1 : Un = 110 V (phase-to-phase voltage)

When the relay is expected to trip at a generator reverse power of 6 %, calculation of the setting value is as follows:

$$P_{R>} (\%) = \frac{\frac{1875 \text{ kVA. } 0.8}{\sqrt{3.20.100}}}{100\text{V.5A}} .6(\%) = 5 \%$$

According to the above example, the *IRP1* has to be set to 5 % so that it trips at a generator reverse power of 6 % (rated generator active power).

Connection of the *IRP1* to phase-toneutral voltage

Conversion of the generator phase power P_{GS} based on the transformer secondary side:

$$\mathsf{P}_{\rm GS} = \frac{\mathsf{S}_{\rm G}.\,\cos\,(\boldsymbol{\varphi})}{\sqrt{3}.\mathsf{n}_{\rm u}.\mathsf{n}_{\rm i}}$$

With the permissible generator reverse power $\rm P_{\rm \tiny RG}$, the setting value $\rm P_{\rm \tiny R}$ is then calculated as follows:

$$P_{R>} (\%) = \frac{\frac{S_{G} \cdot \cos (\phi)}{3.n_{u} \cdot n_{i}}}{U_{n} \cdot I_{n}} \cdot P_{RG}(\%)$$

Calculation example 2: Low voltage 400 V, connectionto-phase voltage

- generator apparent power: S_G = 625 kVA
- rated power factor: $\cos(\phi) = 0.8$
- rated current of IRP1 : $I_n = 5 A$
- rated voltage of *IRP1* : U_n = 230 V (phase-to-neutral voltage)
- transformation ratio of the CT: $n_1 = 1000 \text{ A/5 A}$
- no VT required

When the relay is expected to trip at a generator reverse power $P_{_{RG}}$ of 5 %, calculation of the setting value $P_{_{R>}}$ is as follows:

$$P_{R>} (\%) = \frac{\frac{625 \text{ kVA. } 0.8}{3.1.200}}{230 \text{ V.5A}} .5(\%) = 3.6\% = 4 \%$$

According to the above example, the IRP1 has to be set to 4 % so that it trips at a generator reverse power of 5 % (rated generator active power).

6 Operations and settings

6.1 Setting of the parameters by means of DIP-switches

All DIP-switches required for setting of the parameters are located on the front plate.

6.1.1 Setting of the pickup value

The pickup values for reverse power tripping P_{R1} or P_{R2} can be adjusted by the DIP switches in a range from 2% to 17.5 % P_{N} in 0.5 % steps. The pickup value is calculated from the total of all DIP switch positions.

Example:

A pickup value $\mathrm{P}_{_{R1}}$ of 5.5 % of the rated power is to be adjusted

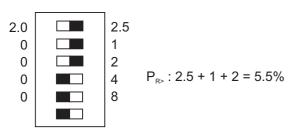


Fig. 6.1:Adjustment example

6.1.2 Setting of the trip delays

The trip delays t_{PR1} and t_{PR2} can be adjusted by the DIP switches in a range from 0.1 s to 62 s with a grading of 0.1 s or 2 s. The pickup value is calculated from the total of all DIP switch positions.

Example:

A delay time of 14 s is to be adjusted:

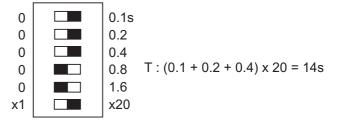


Fig. 6.2: Setting of the delay times

6.2 Fault indication

There are four LEDs at the front plate of the *IRP1* for indicating faults. The pickup LEDs above P_{R1} and P_{R2} light up yellow, and LEDs below P_{R1} and P_{R2} light up red when the respective output relay trips.

6.3 Reset

6.3.1 Manual reset

When the <RESET> push button is pressed, the trip relay is reset and the LED indication extinguishes. This on condition that all code jumpers are unpluged.

6.3.2 Automatic reset

Code jumpers 1 and 3:

The yellow and red fault indications (LED P_{R1} and P_{R2}) are coded for latching if the code jumpers are not applied to sockets 1 and 3. Therefore any fault indication can only be reset manually by pressing the <RESET> push button.

If the code jumpers are applied to sockets 1 and 3, the fault indication is automatically reset as soon as the fault is removed.

Code jumpers 2 and 4:

The trip relays are coded for latching if the code jumpers are not applied to sockets 2 and 4. Therefore any fault indication can only be reset manually by pressing the <RESET> push button. If the code jumpers are applied to sockets 2 and 4, the fault indication is automatically reset as soon as the fault is removed.

7 Housing

The *IRP1* can be supplied in an individual housing for flush-mounting or as a plug-in module for installation in a 19" mounting rack according to DIN 41494. Both versions have plug-in connections.

Relays of variant D are complete devices for flush mounting, whereas relays of variant A are used for 19" rack mounting. Housing variant A to be installed in switchboards of protection class IP51. For switchboards of lower protection classes housing variant D can be used.

7.1 Individual housing

The individual housing of the *IRP1* is constructed for flush-mounting. The dimensions of the mounting frame correspond to the requirements of DIN 43700 (76 \times 142 mm). The cut-out for mounting is 68.7 \times 136.5 mm.

The front of the *IRP1* is covered with a transparent, sealable flap (IP54).

For case dimensions and cut-out refer to "technical data". The individual housing is fixed with the supplied clasps from the rear of the switchboard panel.

7.2 Rack mounting

The *IRP1* is in general suitable for installation in a modular carrier according to DIN 41494. The installation dimensions are: 12 TE; 3 HE.

According to requirements, the *IRP1*-devices can be delivered mounted in 19" racks.

If 19" racks are used the panel requires protection class IP51. For switchboards with lower degree of protection must be used individual housing.

7.3 Terminal connections

The plug-in module has a very compact base with plug connectors and screwed-type connectors.

- max. 4 poles screw-type terminals for voltage and current circuits (terminal connectors series A and B with a short time current capability of 500 A / 1 s).
- 27 poles tab terminals for relay outputs, supply voltage etc.(terminal connectors series C, D and E, max. 6 A current carrying capacity). Connection with tabs 6.3 x 0.8 mm for cable up to max. 1.5 mm 2 or with tabs 2.8 x 0.8 mm for cable up to max. 1 mm 2.

By using 2.8 x 0.8 mm tabs a bridge connection between different poles is possible.

The current terminals are equipped with self-closing short-circuit contacts. Thus, the *IRP1* -module can be unplugged even with current flowing, without endangering the current transformers connected.

The following figure shows the terminal block of IRP1

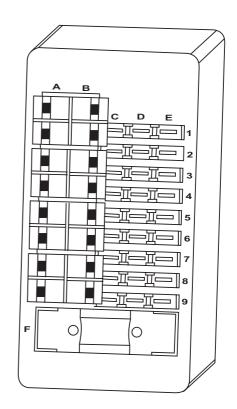


Fig. 7.1: Terminal block of IRP1

8 Relay testing and commissioning

The following test instructions should help to verify the protection relay performance before or during commissioning of the protection system. To avoid a relay damage and to ensure a correct relay operation, be sure that:

- the auxiliary power supply rating corresponds to the auxiliary voltage on site.
- the rated current and rated voltage of the relay correspond to the plant data on site.
- the current transformer circuits are connected to the relay correctly.
- all signal circuits and output relay circuits are connected correctly.

8.1 Power-On

Prior to switch on the auxiliary power supply, be sure that the auxiliary supply voltage corresponds with the rated data on the type plate.

Switch on the auxiliary power supply to the relay (terminals C9/E9) and check that the LED "ON" on the front lights up green.

8.2 Checking the set values

Check all relay set values and see if they are set correctly as you have desired. Set values can be modified by means of the DIP-switches on the front.

8.3 Secondary injection test

8.3.1 Test equipment

- Voltmeter with class 1 or better
- Ammeter with class 1 or better
- Powermeter with class 1 or better
- Auxiliary power supply with the voltage corresponding to the rated data on the type plate
- Single-phase current supply unit (adjustable from 0 to \geq 2.0 x I_N)
- Single-phase voltage source

(adjustable from 0 to $\geq 1.2 \times U_{N}$)

- Timer to measure the operating time
- Switching device
- Test leads and tools

8.3.2 Test circuit

For testing power relays, you need both current and voltage input signals with adjustable phase shifting. Figure 8.1 shows an example of a single phase test circuit with adjustable voltage and current energizing the *IRP1* relay under test.

For testing the power relay, the input voltage shall be applied to the relay via terminals A3/A4. The input current (B3/B4) and phase angle shall be appropriately varied.

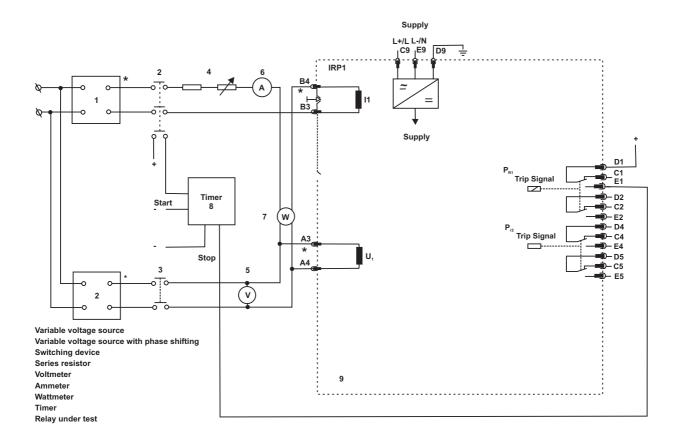


Fig. 8.1: Test circuit

With regard to the right polarity great care must be taken when applying the test current and test voltage to the relay. In figure 8.1 the relay and test source polarity are indicated by a * mark near the terminals. If the voltage and current sources are connected acc. to the above test circuit diagram, the reverse power will be measured correctly.

8.3.3 Checking the operating and resetting values of the relay

A test voltage equal to the rated voltage has to be applied to terminals A3/A4. For checking the operating and resetting values the test current must be increased until the relay picks up. LED PR1 or PR2 lights up.

The deviation of power measurement related to the reading of the power meter must not exceed 5% (refer to 5.1)

The reset value is ascertained by decreasing test current gradually until the relay PR1 or PR2 releases (with the relevant coding, see chapter 6.3.2). The reset value must not exceed 0.95 times the operating value.

8.3.4 Checking the trip delay

To check the trip delay, a timer to is be connected to the trip relay contact. The timer should be started simultaneously with the current injection in the current input circuit and stopped by the trip relay contact. Apply rated voltage to the relay and set the current to a value corresponding to twice the pickup value and inject the current instantaneously. The trip delay measured by timer should have a deviation <3% of the set value or 20 ms (in case of a short trip delay).

8.4 Primary injection test

Generally, a primary injection test could be carried out in the similar manner as the secondary injection test above described. Since the cost and potential hazards are very high for such a test, especially if staged fault tests are intended, primary injection tests are usually limited to very important protective relays in the power system.

8.5 Maintenance

Maintenance testing is generally done on site at regular intervals. These intervals vary among users depending on many factors: e.g. the type of protective relays employed; the importance of the primary equipment being protected; the user's past experience with the relay, etc.

For static relays like *IRP1*, maintenance testing will be performed at least once a year according to the experiences.

9 **Technical Data**

9.1 Measuring input

Rated data:			
Nominal voltage	:	100 V; 230 V; 400 V	
Nominal current I _N	:	1 A or 5 A	
Nominal frequency f _N	:	50/60 Hz	
Thermal withstand capability			
in current circuit	:	dynamic current withstand (half-wave)	250 x I _N
		for 1 s	100 x I _N
		for 10 s	30 x I _N
		continuously	4 x I _N
Thermal withstand capability			
in voltage circuit	:	continuously	2 x U _N
		for 400 V	1.2 x U _N

9.2 Auxiliary voltage

Rated auxiliary voltages U _H	:	24 V	operating range	16 - 60 V AC / 16 - 80 V DC
		110 V	operating range	50 - 270 V AC / 70 - 360 V DC
Power consumption	:	at 24 V	standby approx. 3 W	operating approx. 6 W
		at 110 V	standby approx. 3 W	operating approx. 6 W

9.3 General data

Permissible interuption of the		
supply voltage without		
influence on the function	:	50 ms
Dropout to pickup ratio	:	>95 %
Returning time	:	30 ms
Minimum operating time	:	30 ms

9.4 Output relays

The output relays have the following characteristics: : 250 V AC / 1500 VA / continuous current 6 A maximum breaking capacity

for DC-voltage:

	ohmic	L/R = 40 ms	L/R = 70 ms
300 V DC	0.3 A / 90 W	0.2 A / 63 W	0.18 A / 54 W
250 V DC	0.4 A / 100 W	0.3 A / 70 W	0.15 A / 40 W
110 V DC	0.5 A / 55 W	0.4 A / 40 W	0.2 A / 22 W
60 V DC	0.7 A / 42 W	0.5 A / 30 W	0.3 A / 17 W
24 V DC	6 A / 144 W	4.2 A / 100 W	2.5 A / 60 W

A (VDE 0435/0972 and IEC 65/VDE 0860/8.86)
x 10 ⁶ operating cycles
x 10 ⁵ operating cycles at 220 V AC / 6 A
ver cadmium oxide (AgCdO)
)

9.5 System data		
Design standard	:	VDE 0435, part 303, IEC 255-4, BS 142
Specified ambient service		
Temperature range for storage for operation	:	- 40°C to + 85°C - 20°C to + 70°C
Environmental protection class F as per DIN 40040 and per DIN IEC 68 2-3		relative humidity 95 % at 40°C for 56 days
High voltage tests :		
Insulation test voltage, inputs and outputs between themselves and to the relay frame as per VDE 0435, part 303; IEC 255-5	:	2.5 kV (eff.), 50 Hz; 1 min
Impulse test voltage, inputs and outputs between themselves and to the relay frame as per VDE 0435, part 303; IEC 255-5	:	5 kV; 1.2 / 50 μs; 0.5 J
High frequency interference test voltage, inputs and outputs between themselves and to the relay frame as per DIN IEC 255-6	:	2.5 kV / 1MHz
Electrical fast transient (Burst) test as per DIN VDE 0843, part 4; IEC 801-4	:	4 kV / 2.5 kHz, 15 ms
Radio interference suppression test as per DIN VDE 57 871 Electrostatic discharge (ESD) test as per DIN VDE 0843 part 2	:	limit value class B
IEC 801-2	:	8 kV
Radiated electromagnetic field test as per VDE 0843 part 3; IEC 801-2	:	electrical field strength 10 V/m
Mechanical tests:		
Shock Vibration Degree of protection	: : :	class 1 acc. to DIN IEC 255 part 21-2 class 1 acc. to DIN IEC 255 part 21-1 IP54 by enclosure of the relay case and front panel (relay version D)
Weight	:	approx. 1.5 kg
Pollution degree	:	2 where design A is used

3 where design D is used

Overvoltage class :

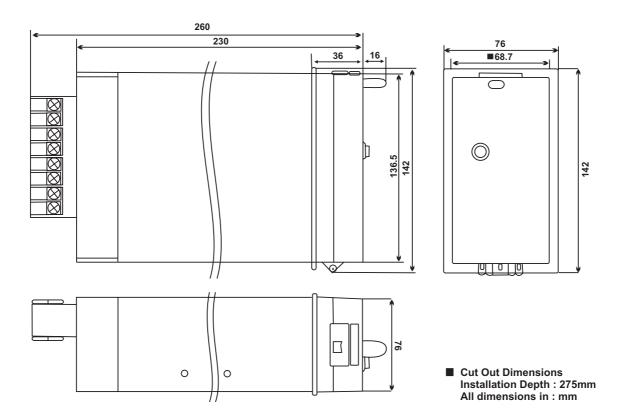
Influencing parameters:

Frequency	:	40 Hz $<$ f $<$ 70 Hz: $<3\%$ of the set value
Temperature	:	-20°C bis +70°C
Aux. voltage	:	no influence in the permissible range

9.6 Setting ranges and graduation

Parameter	Setting range	Graduation	Tolerance
$P_{_{R1}}$ and $P_{_{R2}}$	2% 17.5% x P _N	0.5%	±5% of setting value
t_{PR1} and t_{PR2}	0.1 s 3.1 s	0.1 s	±3% or ±20 ms
	2.0 s 62 s	2.0 s	

9.7 Dimensional drawing



Please observe:

A distance of 50 mm is necessary when the units are mounted one below the other for the housing bonnet to be easily opened. The front cover can be open downwards.

10 Order form

Directional power relay	RP1 -	1	I		U			
Power measuring								
Rated current:	1 A 5 A			1 5				
Rated voltage:	100 V 230 V 400 V					1 2 4		
Auxiliary voltage (AC/DC): 24 V (16 V 1 110 V (50 V						L C) H	
Housing (12TE):	19"- rack Flush moun	ting						A D

For further information, please contact :



C&S Electric Limited

(Protection & Control Division)

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